

Plasma Sheathing Control Using Boundary Layer Stabilization and Additives

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Paper Presented at
AFOSR Workshop on Communications Through Plasma
During Hypersonic Flight

29 August 2006, Boston, MA

Acknowledgement of Support and Disclaimer

This material is based upon work supported by the United States Air Force under Contract Number FA8718-05-C-0054. Any opinions, findings and conclusions or recommendations expressed in this material are those of the author(s) and do not necessarily reflect the views of the United States Air Force.

Report Documentation Page			Form Approved OMB No. 0704-0188		
Public reporting burden for the collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to a penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number.					
1. REPORT DATE 29 AUG 2006	2. REPORT TYPE		3. DATES COVERED 00-00-2006 to 00-00-2006		
4. TITLE AND SUBTITLE Plasma Sheathing Control Using Boundary Layer Stabilization and Additives			5a. CONTRACT NUMBER		
			5b. GRANT NUMBER		
			5c. PROGRAM ELEMENT NUMBER		
6. AUTHOR(S)			5d. PROJECT NUMBER		
			5e. TASK NUMBER		
			5f. WORK UNIT NUMBER		
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) Physical Sciences Inc,20 New England Business Center,Andover,MA,01810			8. PERFORMING ORGANIZATION REPORT NUMBER		
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)			10. SPONSOR/MONITOR'S ACRONYM(S)		
			11. SPONSOR/MONITOR'S REPORT NUMBER(S)		
12. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release; distribution unlimited					
13. SUPPLEMENTARY NOTES					
14. ABSTRACT					
15. SUBJECT TERMS					
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT Same as Report (SAR)	18. NUMBER OF PAGES 20	19a. NAME OF RESPONSIBLE PERSON
a. REPORT unclassified	b. ABSTRACT unclassified	c. THIS PAGE unclassified			

Acknowledgment and Note

VG06-206-1

- **This Phase I SBIR effort was sponsored by two AFRL organizations: SNHE and VAAC, with additional interest from a third organization: VSBXT**
- **The technical monitor is Dr. James Ernstmeier of AFRL/SNHE at Hanscom AFB, MA**
- **Special note: This presentation provides a general overview of potential sheathing solutions. Specific results and designs have SBIR rights and ITAR restrictions. The detailed report can be obtained from Dr. Ernstmeier.**



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Outline

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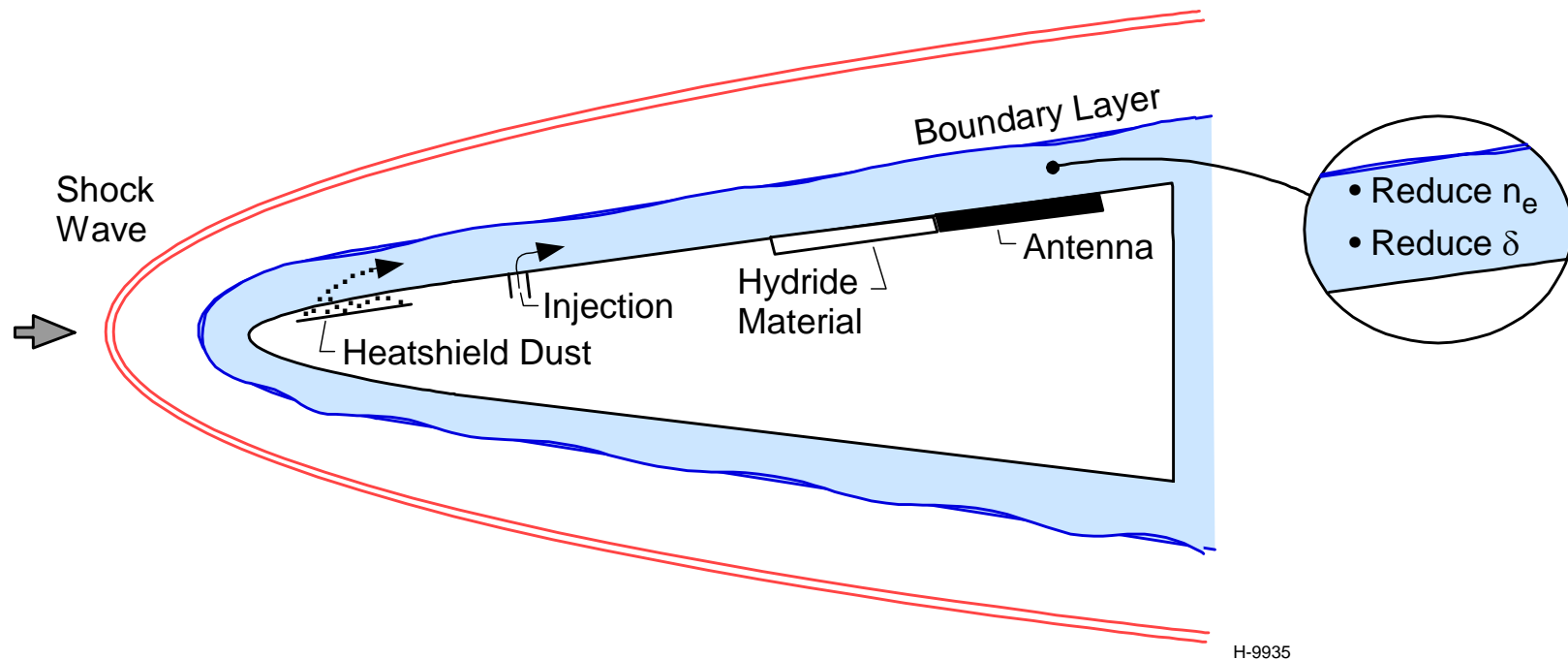
- **Plasma sheathing control objectives**
- **Three techniques**
 - Boundary layer stabilization by extreme cooling
 - Liquid injection into boundary layer flow
 - Electrophilic material in heat shield material
- **Application to hypersonic vehicles**
- **Summary**



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Plasma Sheathing Control Objectives

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- Control sheathing via temperature and chemistry
- Reduce electron density, n_e
- Reduce boundary layer thickness, δ

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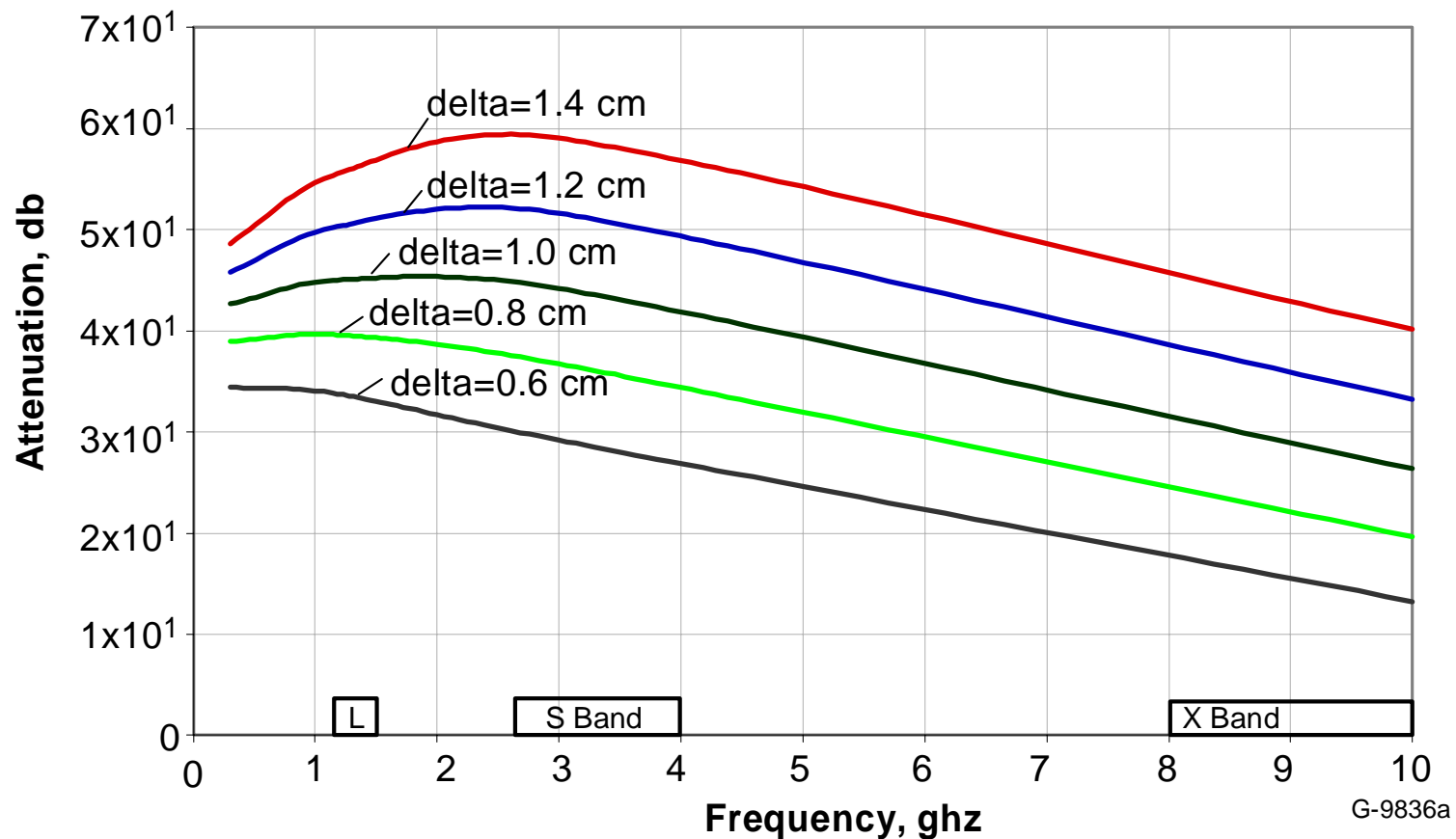
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Plasma Sheath Attenuation Reduction

BRV, 50 kft, $n_e = 1.8 \times 10^{12}/\text{cm}^3$, 0.130 atm, $\nu_c = 1.3 \times 10^{10} \text{ S}^{-1}$

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Boundary Layer Thickness Reduction



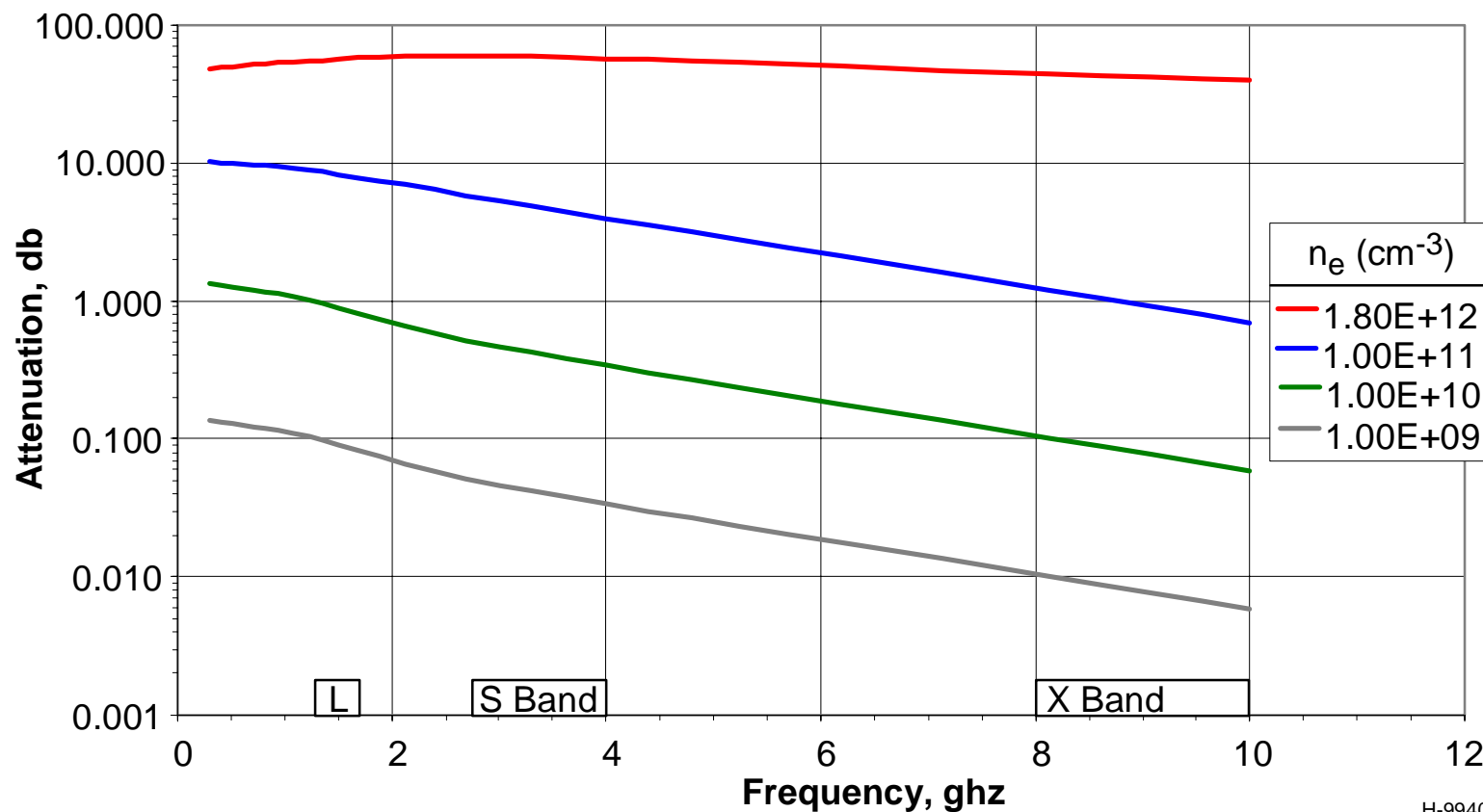
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Plasma Sheath Attenuation Reduction

BRV, 50 kft, Delta = 1.4 cm, 0.130 atm, $\nu_c = 1.3 \times 10^{10} \text{ S}^{-1}$

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Electron Density Reduction



H-9940



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Extreme Surface Cooling Using Hydride Materials

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- **Extreme cooling stabilizes hypersonic boundary layer**
 - Secondary mode unstable at high edge mach number
 - Remain below $M_{e_{2nd\ mode}}$ for laminar flow
- **Hydride cooling works over a large range of heating conditions**
 - Amount of hydride (material thickness) controls “cool time”
- **Hydrogen gas released during low-temperature ablation process**
 - 15-20 kJ/gm H_2 , heat of desorption (and adsorption)

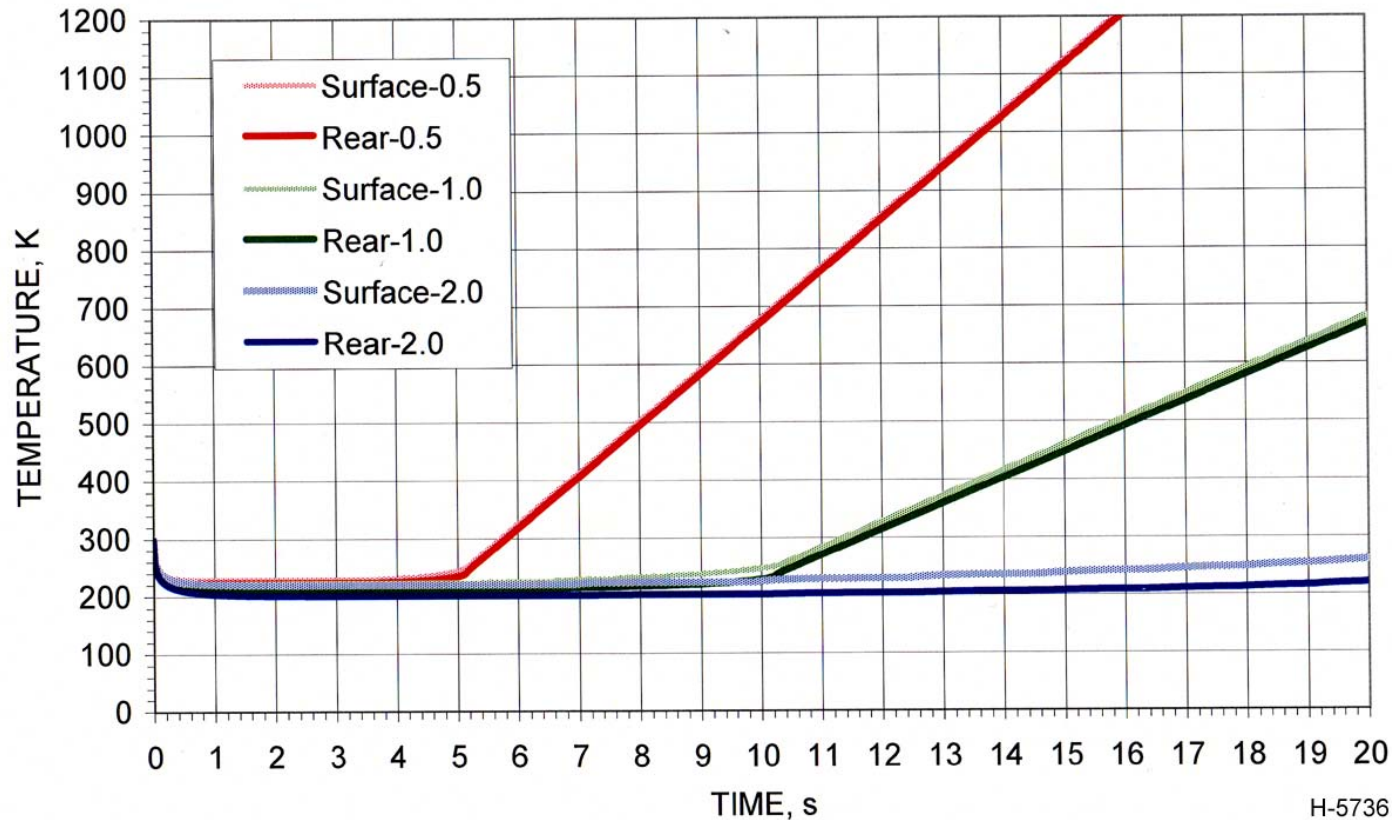
**Hydride cooling works over wide range of
trans-atmospheric flight conditions**



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Hydride Cooling for Typical Surface Heating Flux 50 W/cm²

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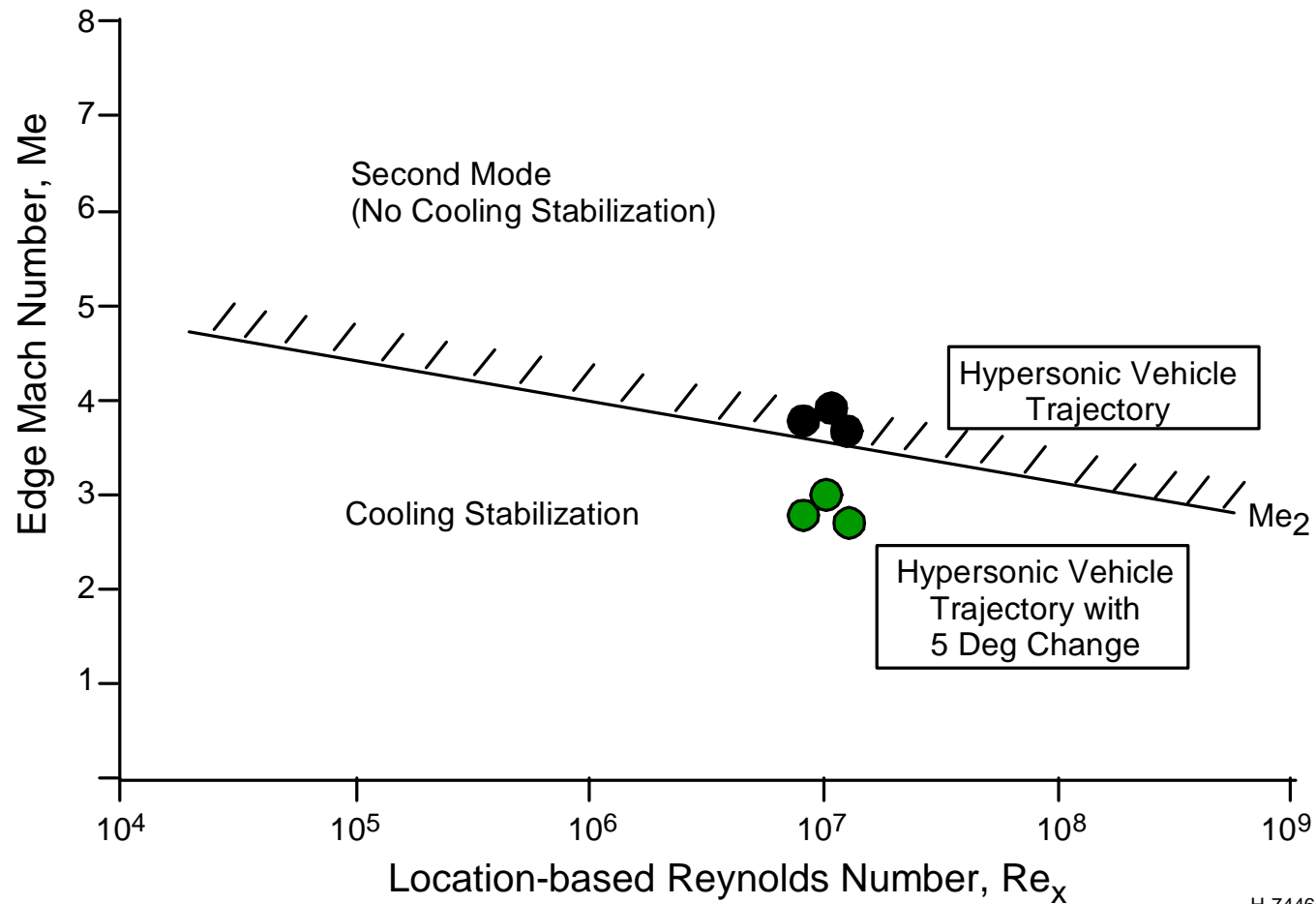
Computations performed using PSI's
validated thermal response code



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Cooling Stabilization Boundary for Trans-atmospheric Trajectory Points

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Liquid Injection

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- **NASA RAM C-III Flight Experiment 1973**
 - $n_e(\text{cm}^{-3})$ at boundary layer standoff distance 4 cm, 71-72 km altitude
 - No injection: 3.9×10^{10}
 - Water: 4.8×10^9
 - Freon-3: 3.8×10^8
 - Blunt vehicle, Teflon frustum, 5000 ppm alkali impurities, pulsed injection
- **Employed Non-equilibrium Boundary Layer (NEBL) code to compute effects of injectant on downstream electron density**
 - Same trans-atmospheric flight conditions as hydride
 - Instantaneous vaporization
 - 50 ppm alkali in carbon phenolic heatshield
 - Wall cooling effects

Water injection showed insignificant effects, but Freon-3 resulted in orders of magnitude n_e reduction depending on boundary layer cooling

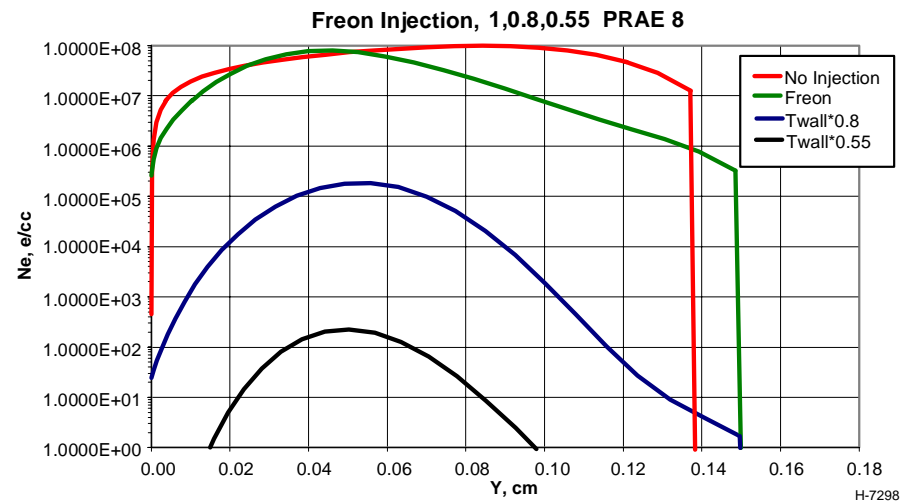


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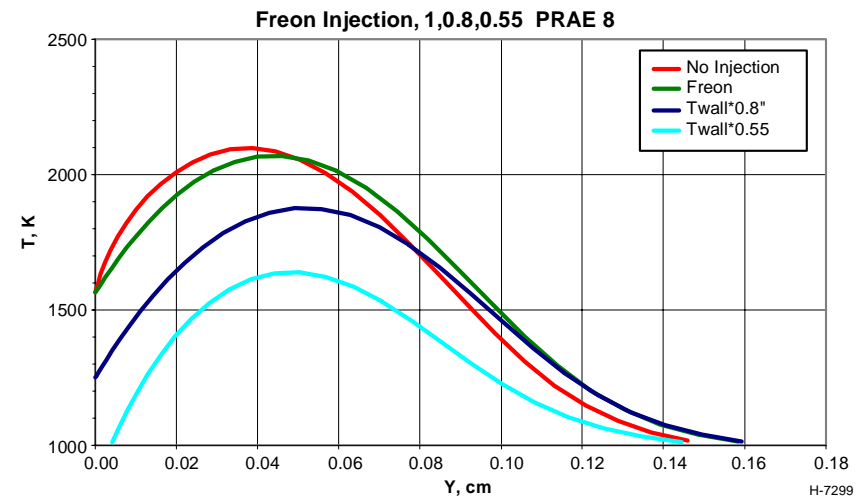
Freon Injection Cases

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$n_e(\text{cm}^{-3})$



$T(^{\circ}\text{K})$



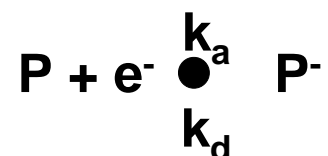
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Heatshield Electrophilic Scavenging Computations

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- Electrophilic particles take up electrons efficiently by the reaction



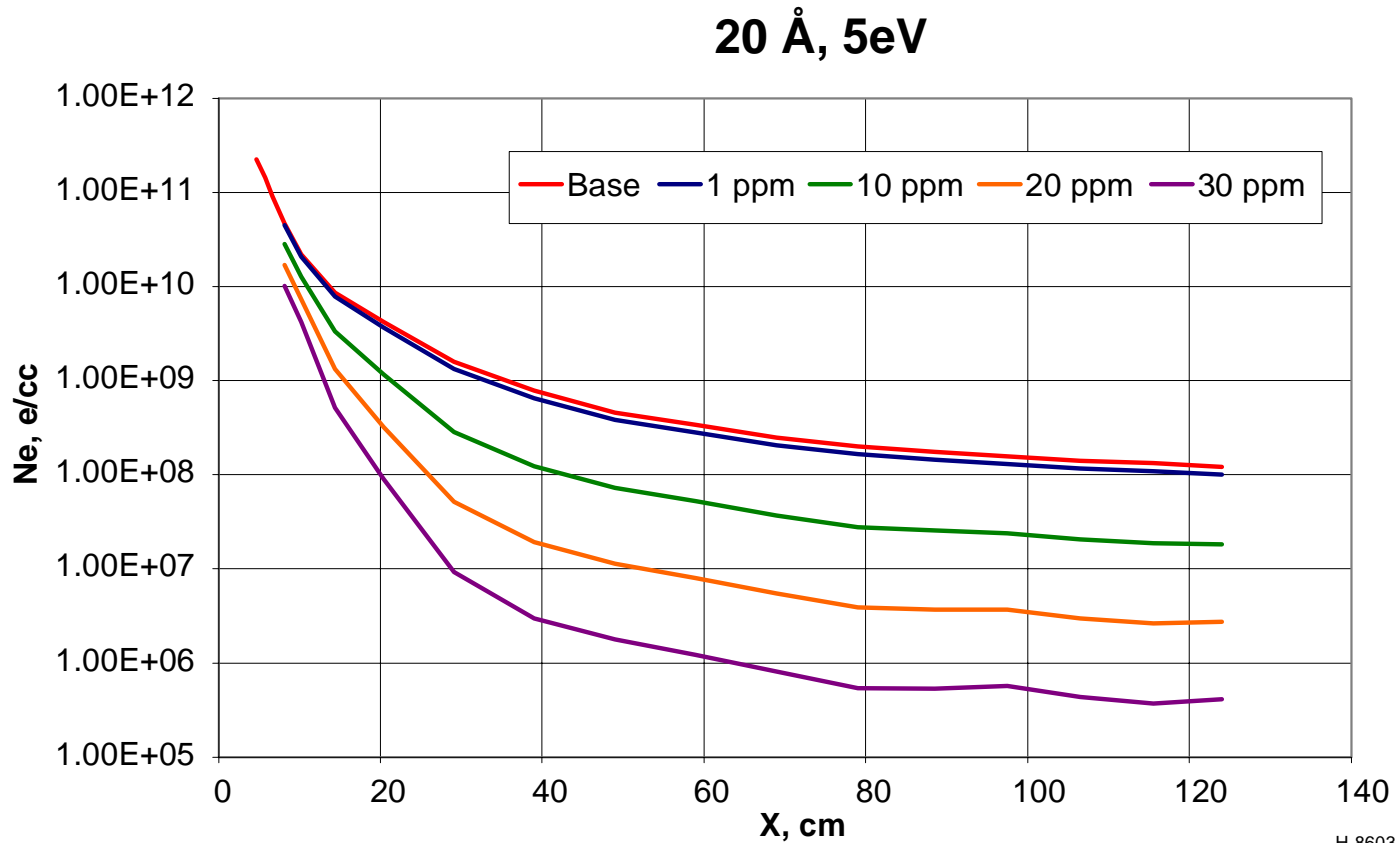
- **Applied heterogeneous chemistry model, Caledonia (1986)**
 - Electrophilic specie concentration (ppm)
 - Particle size (Å)
 - Work function (eV)
 - Temperature (K)



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Electron Density Reduction

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**Large potential sheathing reduction using
low concentration of electrophilic material**



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Vehicle Application

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Requirements	Plasma Sheathing Control Techniques		
	Boundary Layer Transition Control	Additive Injection	Incorporation of Electrophilic Species
Missions			
Weapon	One-time control	Multiple control applications	Continuous
Surveillance	Multiple applications	Multiple control applications	Continuous
Altitude History			
Velocity Time	Velocity dependent 5-20 s	Some velocity dependence 5-20 s, pulse	Some velocity dependence Continuous or pulsed
Configuration			
Waverider	Compatible	Compatible	Compatible, distributed in heatshield or injected
Bi-conic	Compatible	Compatible	Compatible, distributed in heatshield or injected
Design			
• Volume Impact	Small	Modest	Very small
• Weight Impact	Small	Modest	Very small
• Power Impact	Very small	Small	None, small if injected



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Summary

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- **Three general techniques to control plasma sheathing have been identified.**
- **All three schemes are potentially viable for application to hypersonic cruise vehicles.**
- **Experimental validation and multi-phase modeling simulations are needed to pursue this promising technology further.**



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Backup Charts

Metallic Hydrides

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- Transition metal hydrides**

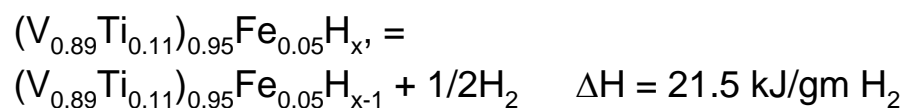
- $A_x B_{1-x} H_y$ type compounds
- decompose rapidly and endothermically to produce H_2



Heats of Desorption (and Adsorption)

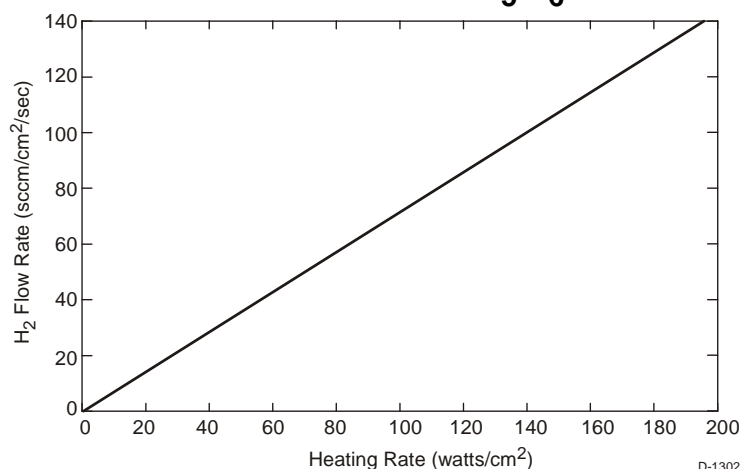


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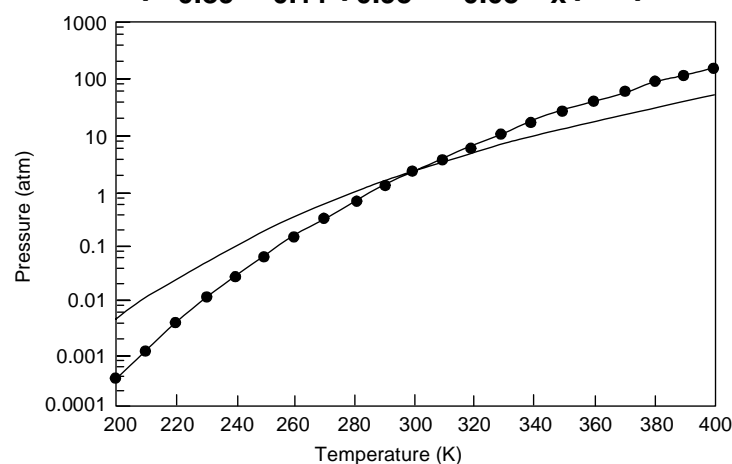


- High energy, low temperature ablators

H_2 Flow as a Function of Heating Rate for $LaNi_5 H_6$



H_2 Pressure Above $LaNi_5 H_6$ (—) and $(V_{0.89} Ti_{0.11})_{0.95} Fe_{0.05} H_x$ (•—•)



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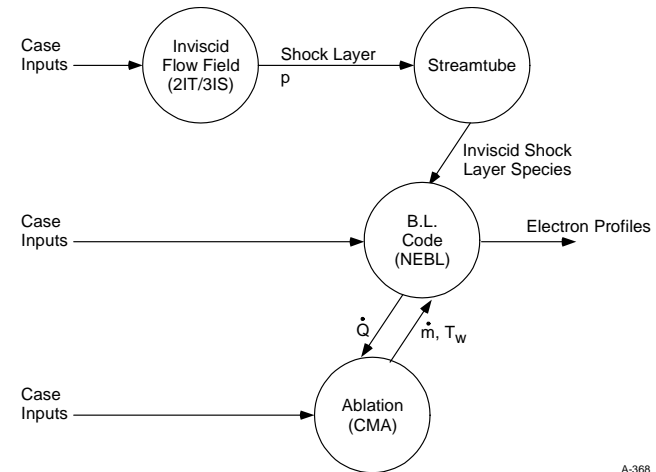
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Boundary Layer Models

- **Non-Equilibrium BL (NEBL) Code**
 - implicit, fully-coupled model
 - unique chemistry models
- **TURBL**
 - 8 equation turbulence model
 - temperature fluctuations mirror plasma behavior
- **REACH (developed by SAIC)**
 - 3D BL Code

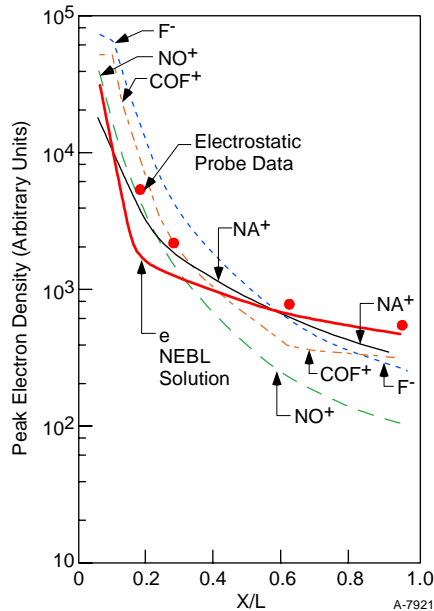
NEBL Methodology

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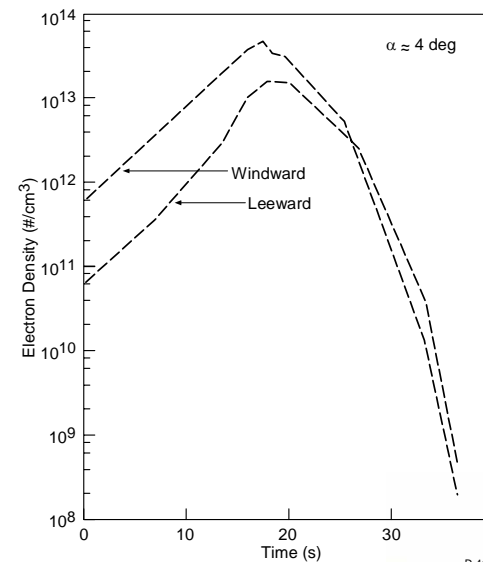
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NEBL Calculation



Teflon
RMV-340
131 kft

REACH Simulation



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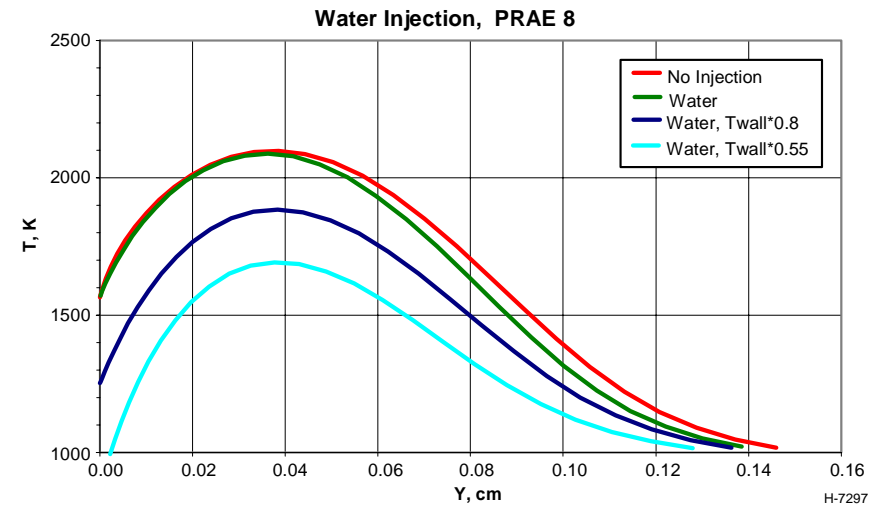
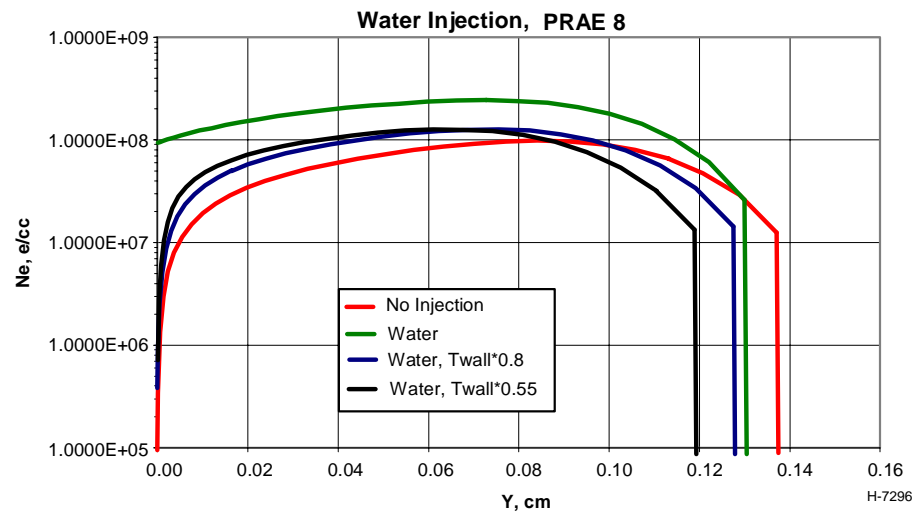
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Water Injection Cases

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$n_e(\text{cm}^{-3})$

$T(^{\circ}\text{K})$



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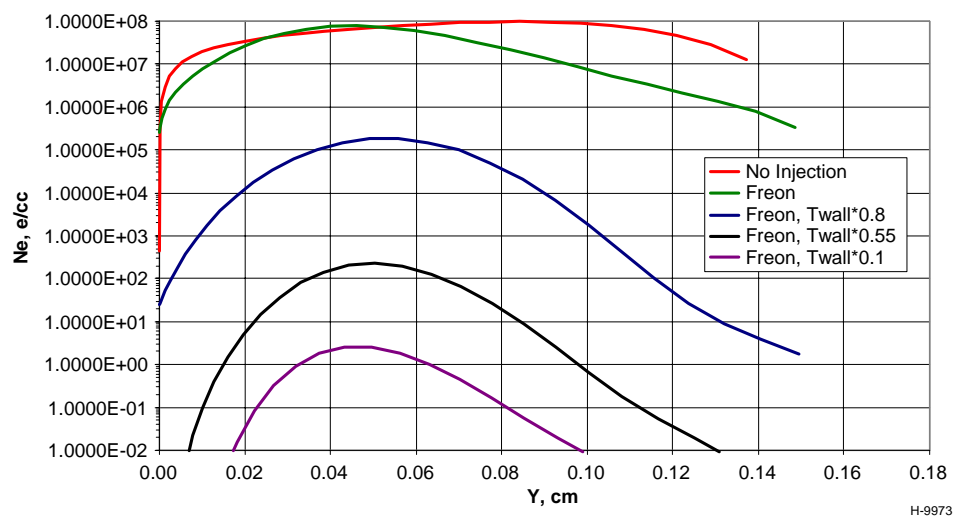
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Freon Injection

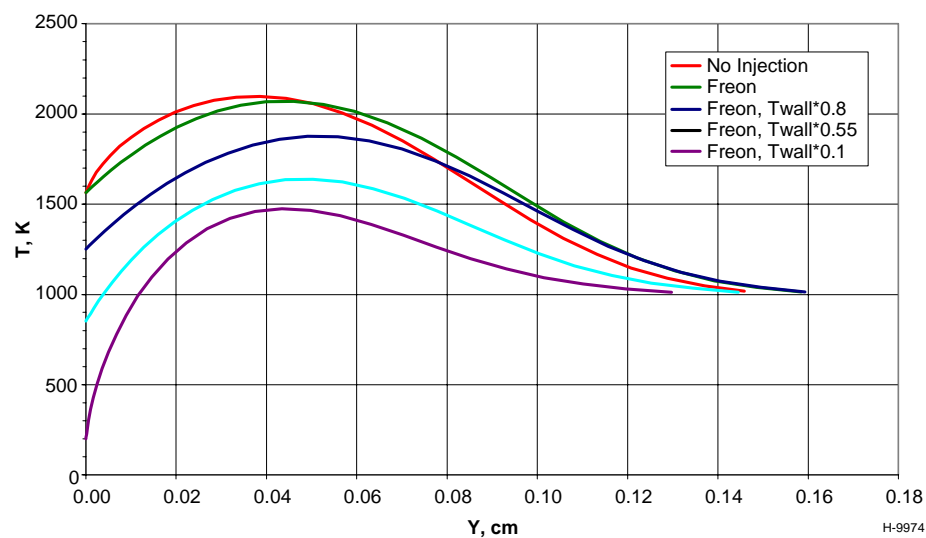
Synergistic Effects: Hydride Cooling and Injection

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$n_e(\text{cm}^{-3})$



$T(^{\circ}\text{K})$



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